

## High-Precision, Low-Noise, Rail-to-Rail Output, 11MHz JFET Op Amp

Check for Samples: [OPA140](#), [OPA2140](#), [OPA4140](#)

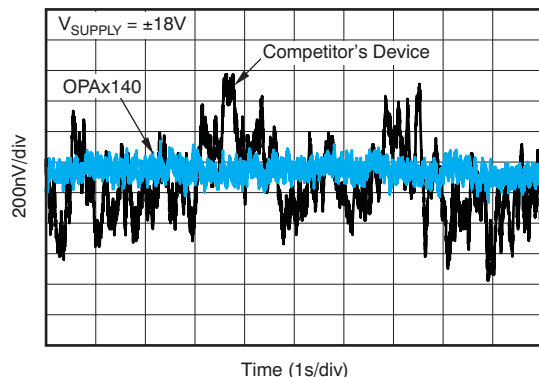
### FEATURES

- **Very Low Offset Drift:** 1 $\mu$ V/ $^{\circ}$ C max
- **Very Low Offset:** 120 $\mu$ V
- **Low Input Bias Current:** 10pA max
- **Very Low 1/f Noise:** 250nV<sub>PP</sub>, 0.1Hz to 10Hz
- **Low Noise:** 5.1nV/ $\sqrt{\text{Hz}}$
- **Slew Rate:** 20V/ $\mu$ s
- **Low Supply Current:** 2.0mA max
- **Input Voltage Range Includes V<sub>-</sub> Supply**
- **Single-Supply Operation:** 4.5V to 36V
- **Dual-Supply Operation:**  $\pm$ 2.25V to  $\pm$ 18V
- **No Phase Reversal**
- **Industry-Standard SO Packages**
- **MSOP-8, TSSOP, and SOT23 Packages**

### APPLICATIONS

- **Battery-Powered Instruments**
- **Industrial Controls**
- **Medical Instrumentation**
- **Photodiode Amplifiers**
- **Active Filters**
- **Data Acquisition Systems**
- **Automatic Test Systems**

#### 0.1Hz to 10Hz NOISE



### DESCRIPTION

The OPA140, OPA2140, and OPA4140 op amp family is a series of low-power JFET input amplifiers that feature good drift and low input bias current. The rail-to-rail output swing and input range that includes V<sub>-</sub> allow designers to take advantage of the low-noise characteristics of JFET amplifiers while also interfacing to modern, single-supply, precision analog-to-digital converters (ADCs) and digital-to-analog converters (DACs).

The OPA140 achieves 11MHz unity-gain bandwidth and 20V/ $\mu$ s slew rate while consuming only 1.8mA (typ) of quiescent current. It runs on a single 4.5 to 36V supply or dual  $\pm$ 2.25V to  $\pm$ 18V supplies.

All versions are fully specified from  $-40^{\circ}$ C to  $+125^{\circ}$ C for use in the most challenging environments. The OPA140 (single) is available in the SOT23-5, MSOP-8, and SO-8 packages; the OPA2140 (dual) is available in both MSOP-8 and SO-8 packages; and the OPA4140 (quad) is available in the SO-14 and TSSOP-14 packages.

### RELATED PRODUCTS

FEATURES	PRODUCT
Low-Power, 10MHz FET Input Industrial Op Amp	<a href="#">OPA141</a>
2.2nV/ $\sqrt{\text{Hz}}$ , Low-Power, 36V Operational Amplifier in SOT23 Package	<a href="#">OPA209</a>
Low-Noise, High-Precision, 22MHz, 4nV/ $\sqrt{\text{Hz}}$ JFET-Input Operational Amplifier	<a href="#">OPA827</a>
Low-Noise, Low I <sub>Q</sub> Precision CMOS Operational Amplifier	<a href="#">OPA376</a>
High-Speed, FET-Input Operational Amplifier	<a href="#">OPA132</a>



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This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

### ABSOLUTE MAXIMUM RATINGS<sup>(1)</sup>

Over operating free-air temperature range (unless otherwise noted).

		VALUE	UNIT
Supply Voltage		±20	V
Signal Input Terminals	Voltage <sup>(2)</sup>	(V–) –0.5 to (V+) +0.5	V
	Current <sup>(2)</sup>	±10	mA
Output Short-Circuit <sup>(3)</sup>		Continuous	
Operating Temperature, T <sub>A</sub>		–55 to +150	°C
Storage Temperature, T <sub>A</sub>		–65 to +150	°C
Junction Temperature, T <sub>J</sub>		+150	°C
ESD Ratings	Human Body Model (HBM)	2000	V
	Charged Device Model (CDM)	500	V

- (1) Stresses above these ratings may cause permanent damage. Exposure to absolute maximum conditions for extended periods may degrade device reliability. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those specified is not supported.
- (2) Input terminals are diode-clamped to the power-supply rails. Input signals that can swing more than 0.5V beyond the supply rails should be current limited to 10 mA or less.
- (3) Short-circuit to V<sub>S</sub>/2 (ground in symmetrical dual-supply setups), one amplifier per package.

### PACKAGE INFORMATION<sup>(1)</sup>

PRODUCT	PACKAGE-LEAD	PACKAGE DESIGNATOR	PACKAGE MARKING
OPA140	SO-8	D	OPA140
	MSOP-8	DGK	140
	SOT23-5	DBV	O140
OPA2140	SO-8	D	O2140A
	MSOP-8	DGK	2140
OPA4140	TSSOP-14	PW	O4140A
	SO-14	D	O4140A

- (1) For the most current package and ordering information see the Package Option Addendum at the end of this document, or visit the device product folder at [www.ti.com](http://www.ti.com).

**ELECTRICAL CHARACTERISTICS:  $V_S = +4.5V$  to  $+36V$ ;  $\pm 2.25V$  to  $\pm 18V$** 
**Boldface** limits apply over the specified temperature range,  $T_A = -40^\circ\text{C}$  to  $+125^\circ\text{C}$ .

 At  $T_A = +25^\circ\text{C}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

PARAMETER	CONDITIONS	OPA140, OPA2140, OPA4140			UNIT
		MIN	TYP	MAX	
<b>OFFSET VOLTAGE</b>					
Offset Voltage, RTI	$V_{OS}$	$V_S = \pm 18V$	30	120	$\mu\text{V}$
<b>Over Temperature</b>		$V_S = \pm 18V$		<b>220</b>	$\mu\text{V}$
<b>Drift</b>	$dV_{OS}/dT$	$V_S = \pm 18V$	<b><math>\pm 0.35</math></b>	<b>1.0</b>	$\mu\text{V}/^\circ\text{C}$
vs Power Supply	PSRR	$V_S = \pm 2.25V$ to $\pm 18V$	$\pm 0.1$	$\pm 0.5$	$\mu\text{V}/\text{V}$
<b>Over Temperature</b>		$V_S = \pm 2.25V$ to $\pm 18V$		<b><math>\pm 4</math></b>	$\mu\text{V}/\text{V}$
<b>INPUT BIAS CURRENT<sup>(1)</sup></b>					
Input Bias Current	$I_B$		$\pm 0.5$	$\pm 10$	pA
<b>Over Temperature</b>				<b><math>\pm 3</math></b>	<b>nA</b>
Input Offset Current	$I_{OS}$		$\pm 0.5$	$\pm 10$	pA
<b>Over Temperature</b>				<b><math>\pm 1</math></b>	<b>nA</b>
<b>NOISE</b>					
Input Voltage Noise					
$f = 0.1\text{Hz}$ to $10\text{Hz}$			250		$\text{nV}_{PP}$
$f = 0.1\text{Hz}$ to $10\text{Hz}$			42		$\text{nV}_{RMS}$
Input Voltage Noise Density	$e_n$				
$f = 10\text{Hz}$			8		$\text{nV}/\sqrt{\text{Hz}}$
$f = 100\text{Hz}$			5.8		$\text{nV}/\sqrt{\text{Hz}}$
$f = 1\text{kHz}$			5.1		$\text{nV}/\sqrt{\text{Hz}}$
Input Current Noise Density	$I_n$				
$f = 1\text{kHz}$			0.8		$\text{fA}/\sqrt{\text{Hz}}$
<b>INPUT VOLTAGE RANGE</b>					
<b>Common-Mode Voltage Range</b>	$V_{CM}$		<b>(V-) -0.1</b>	<b>(V+) -3.5</b>	<b>V</b>
Common-Mode Rejection Ratio	CMRR	$V_S = \pm 18V$ , $V_{CM} = (V-) -0.1V$ to $(V+) -3.5V$	126	140	dB
<b>Over Temperature</b>		$V_S = \pm 18V$ , $V_{CM} = (V-) -0.1V$ to $(V+) -3.5V$	<b>120</b>		<b>dB</b>
<b>INPUT IMPEDANCE</b>					
Differential			$10^{13} \parallel 10$		$\Omega \parallel \text{pF}$
Common-Mode		$V_{CM} = (V-) -0.1V$ to $(V+) -3.5V$	$10^{13} \parallel 7$		$\Omega \parallel \text{pF}$
<b>OPEN-LOOP GAIN</b>					
Open-Loop Voltage Gain	$A_{OL}$	$V_O = (V-) +0.35V$ to $(V+) -0.35V$ , $R_L = 10\text{k}\Omega$	120	126	dB
		$V_O = (V-) +0.35V$ to $(V+) -0.35V$ , $R_L = 2\text{k}\Omega$	114	126	dB
<b>Over Temperature</b>		$V_O = (V-) +0.35V$ to $(V+) -0.35V$ , $R_L = 2\text{k}\Omega$	<b>108</b>		<b>dB</b>
<b>FREQUENCY RESPONSE</b>					
Gain Bandwidth Product	BW		11		MHz
Slew Rate			20		$\text{V}/\mu\text{s}$
Settling Time, 12-bit (0.024)			880		ns
Settling Time, 16-bit			1.6		$\mu\text{s}$
THD+N		1kHz, $G = 1$ , $V_O = 3.5V_{RMS}$	0.00005		%
Overload Recovery Time			600		ns

 (1) High-speed test,  $T_A = T_J$ .

**ELECTRICAL CHARACTERISTICS:  $V_S = +4.5V$  to  $+36V$ ;  $\pm 2.25V$  to  $\pm 18V$  (continued)**

**Boldface** limits apply over the specified temperature range,  $T_A = -40^\circ C$  to  $+125^\circ C$ .

At  $T_A = +25^\circ C$ ,  $R_L = 2k\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} =$  midsupply, unless otherwise noted.

PARAMETER	CONDITIONS	OPA140, OPA2140, OPA4140			UNIT	
		MIN	TYP	MAX		
<b>OUTPUT</b>						
Voltage Output	$V_O$	$R_L = 10k\Omega, A_{OL} \geq 108dB$	$(V-)+0.2$		$(V+)-0.2$	V
		$R_L = 2k\Omega, A_{OL} \geq 108dB$	$(V-)+0.35$		$(V+)-0.35$	V
Short-Circuit Current	$I_{SC}$	Source		+36		mA
		Sink		-30		mA
Capacitive Load Drive	$C_{LOAD}$		See Figure 20 and Figure 21			
Open-Loop Output Impedance	$R_O$	$f = 1MHz, I_O = 0$ (See Figure 19)		16		$\Omega$
<b>POWER SUPPLY</b>						
Specified Voltage Range	$V_S$		$\pm 2.25$		$\pm 18$	V
Quiescent Current (per amplifier)	$I_Q$	$I_O = 0mA$		1.8	2.0	mA
			<b>Over Temperature</b>			<b>2.7</b>
<b>CHANNEL SEPARATION</b>						
Channel Separation		At dc		0.02		$\mu V/V$
		At 100kHz		10		$\mu V/V$
<b>TEMPERATURE RANGE</b>						
Specified Range			-40		+125	$^\circ C$
Operating Range			-55		+150	$^\circ C$

**THERMAL INFORMATION**

THERMAL METRIC <sup>(1)</sup>		OPA140, OPA2140	OPA140, OPA2140	OPA140	UNITS
		D (SO)	DGK (MSOP)	DBV (SOT23)	
		8	8	5	
$\theta_{JA}$	Junction-to-ambient thermal resistance	160	180	210	$^\circ C/W$
$\theta_{JC(top)}$	Junction-to-case(top) thermal resistance	75	55	200	
$\theta_{JB}$	Junction-to-board thermal resistance	60	130	110	
$\psi_{JT}$	Junction-to-top characterization parameter	9	n/a	40	
$\psi_{JB}$	Junction-to-board characterization parameter	50	120	105	
$\theta_{JC(bottom)}$	Junction-to-case(bottom) thermal resistance	n/a	n/a	n/a	

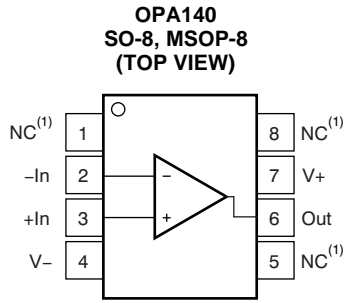
(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

**THERMAL INFORMATION**

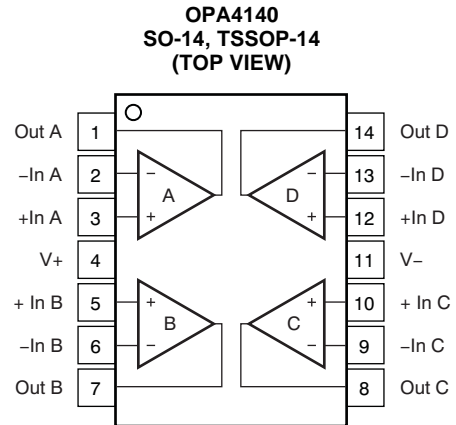
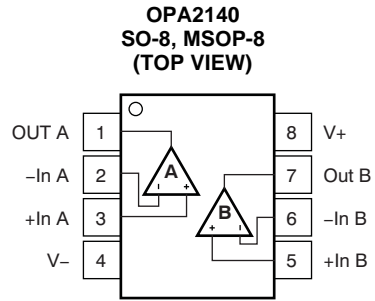
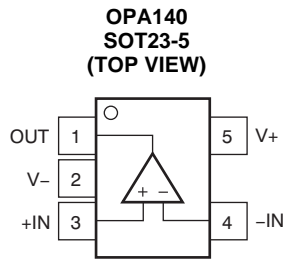
THERMAL METRIC <sup>(1)</sup>		OPA4140	OPA4140	UNITS
		D (SO)	PW (TSSOP)	
		14	14	
$\theta_{JA}$	Junction-to-ambient thermal resistance	97	135	$^\circ C/W$
$\theta_{JC(top)}$	Junction-to-case(top) thermal resistance	56	45	
$\theta_{JB}$	Junction-to-board thermal resistance	53	66	
$\psi_{JT}$	Junction-to-top characterization parameter	19	n/a	
$\psi_{JB}$	Junction-to-board characterization parameter	46	60	
$\theta_{JC(bottom)}$	Junction-to-case(bottom) thermal resistance	n/a	n/a	

(1) For more information about traditional and new thermal metrics, see the *IC Package Thermal Metrics* application report, [SPRA953](#).

PIN ASSIGNMENTS



(1) NC denotes no internal connection.



SIMPLIFIED BLOCK DIAGRAM

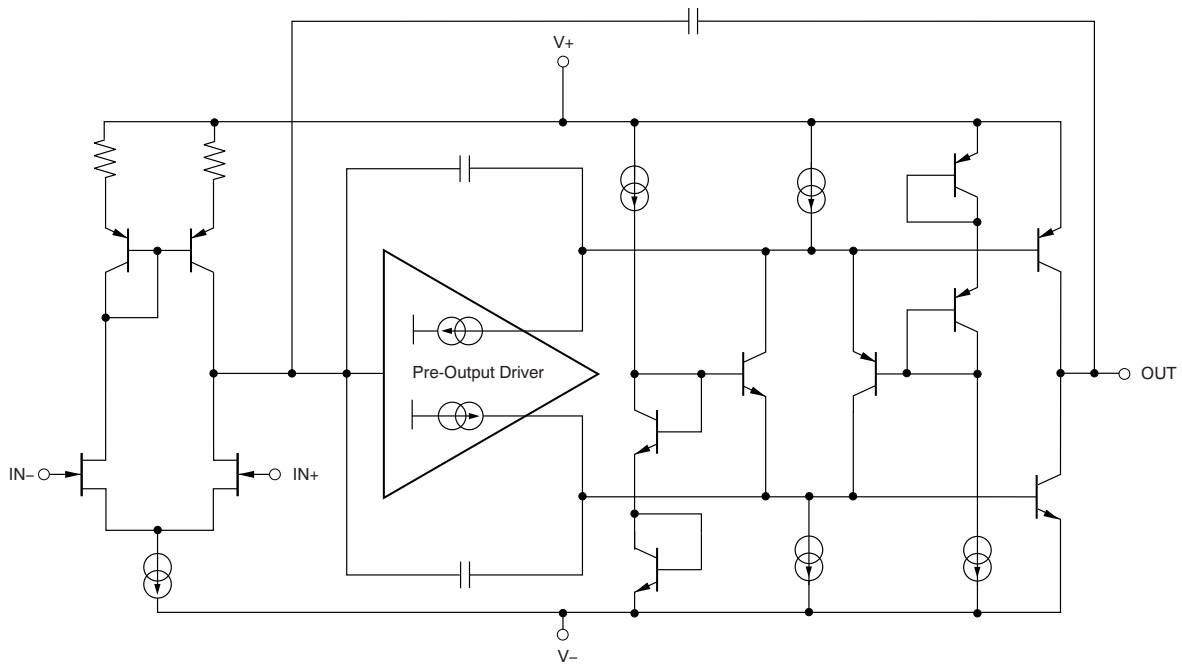


Figure 1.

## TYPICAL CHARACTERISTICS SUMMARY

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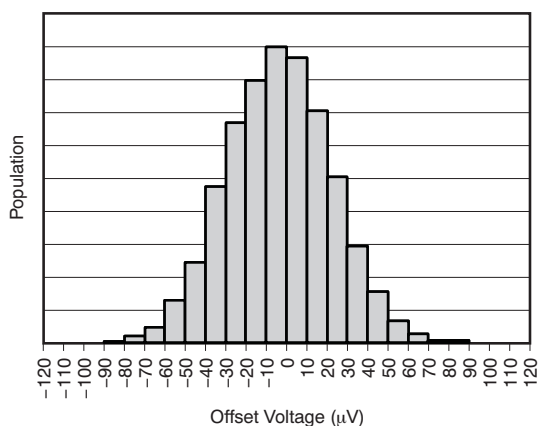
**Table 1. Characteristic Performance Measurements**

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### TYPICAL CHARACTERISTICS

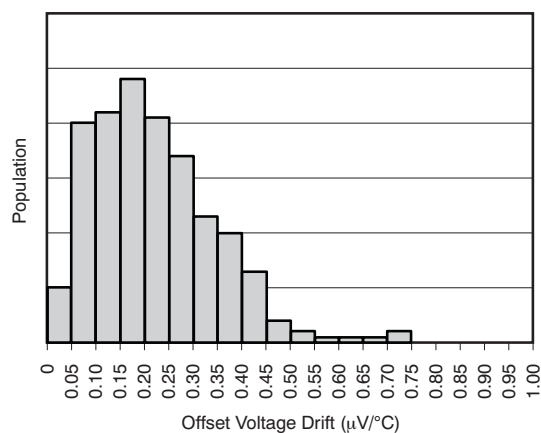
At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

**OFFSET VOLTAGE PRODUCTION DISTRIBUTION**



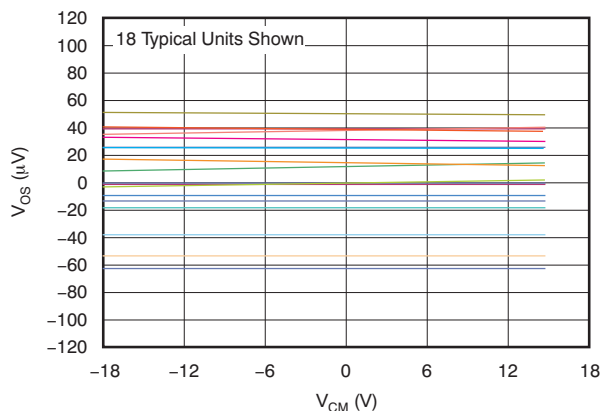
**Figure 2.**

**OFFSET VOLTAGE DRIFT DISTRIBUTION**



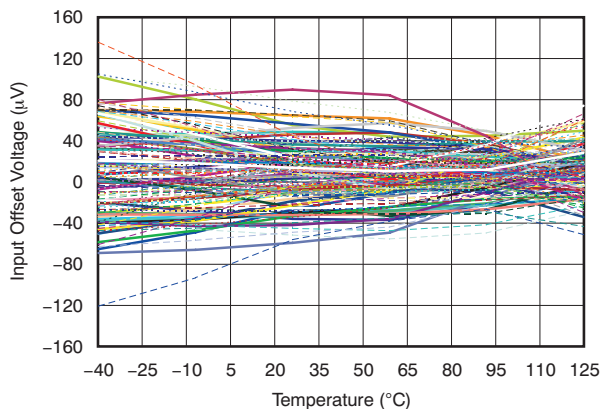
**Figure 3.**

**OFFSET VOLTAGE vs COMMON-MODE VOLTAGE**



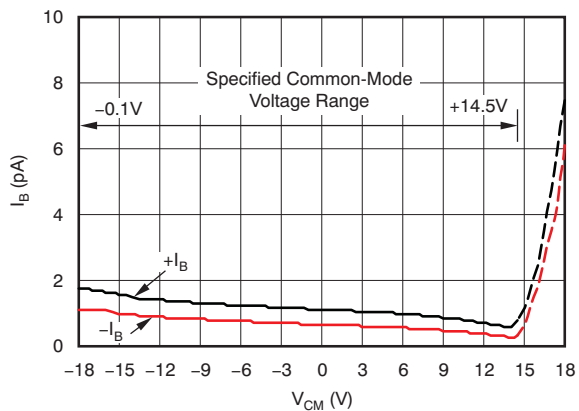
**Figure 4.**

**INPUT OFFSET VOLTAGE vs TEMPERATURE (144 Amplifiers)**



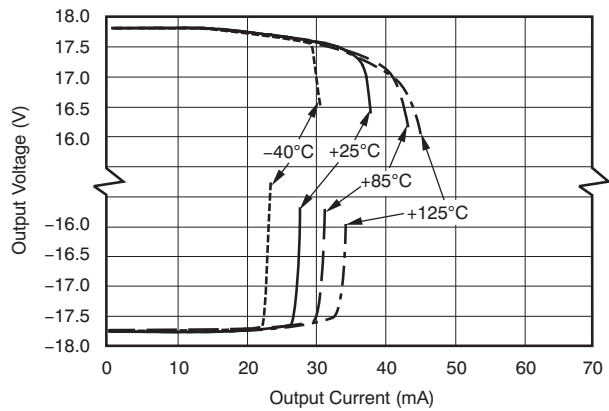
**Figure 5.**

**I<sub>B</sub> vs COMMON-MODE VOLTAGE**



**Figure 6.**

**OUTPUT VOLTAGE SWING vs OUTPUT CURRENT (MAX SUPPLY)**

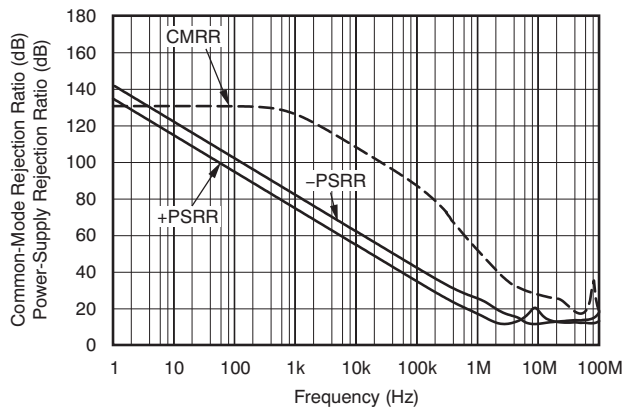


**Figure 7.**

**TYPICAL CHARACTERISTICS (continued)**

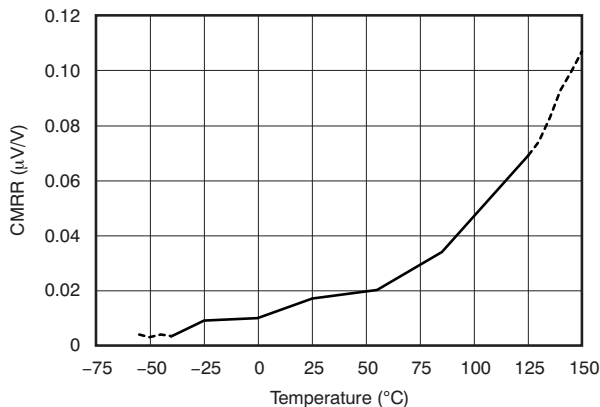
At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

**CMRR AND PSRR vs FREQUENCY (Referred to Input)**



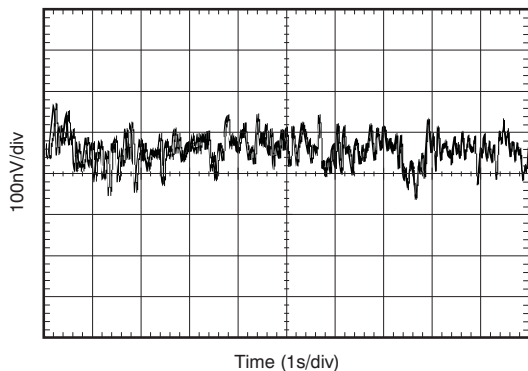
**Figure 8.**

**COMMON-MODE REJECTION RATIO vs TEMPERATURE**



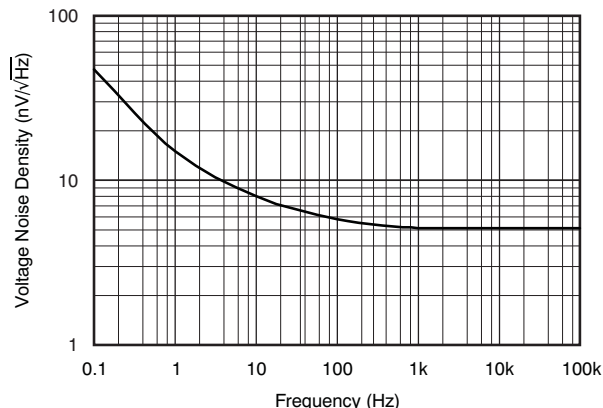
**Figure 9.**

**0.1Hz to 10Hz NOISE**



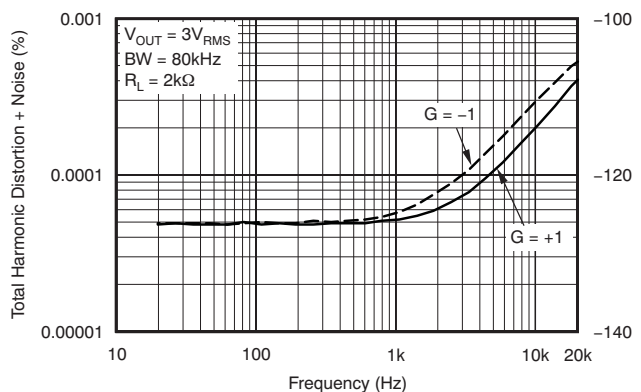
**Figure 10.**

**INPUT VOLTAGE NOISE DENSITY vs FREQUENCY**



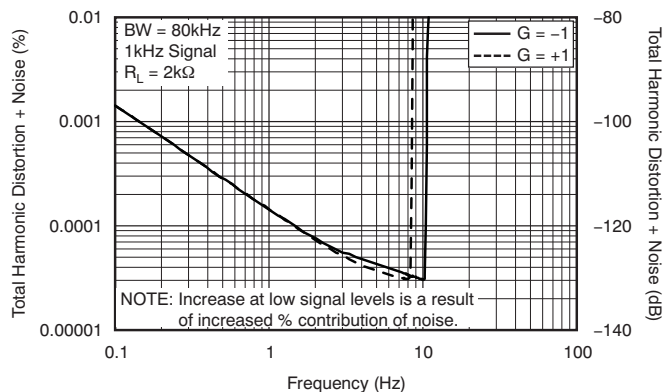
**Figure 11.**

**THD+N RATIO vs FREQUENCY**



**Figure 12.**

**THD+N RATIO vs OUTPUT AMPLITUDE**



**Figure 13.**

**TYPICAL CHARACTERISTICS (continued)**

At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

**QUIESCENT CURRENT vs TEMPERATURE**

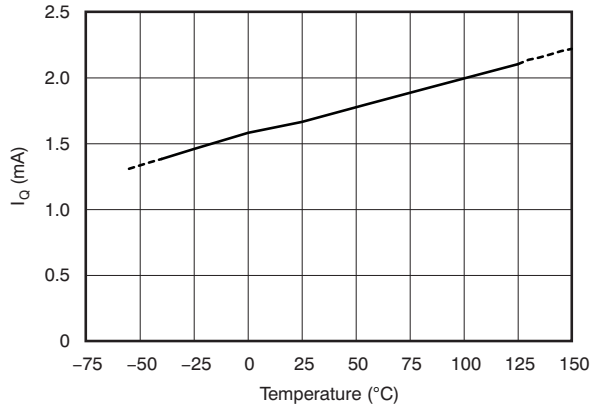


Figure 14.

**QUIESCENT CURRENT vs SUPPLY VOLTAGE**

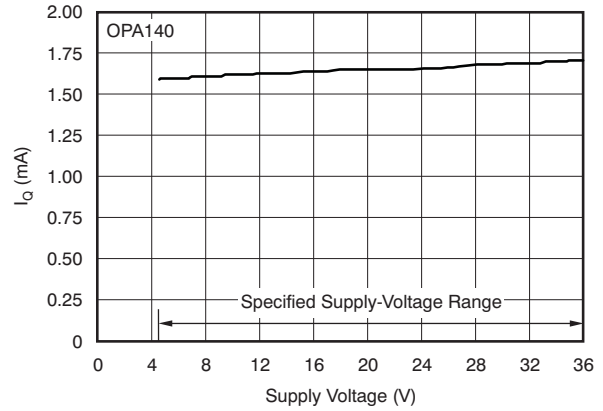


Figure 15.

**GAIN AND PHASE vs FREQUENCY**

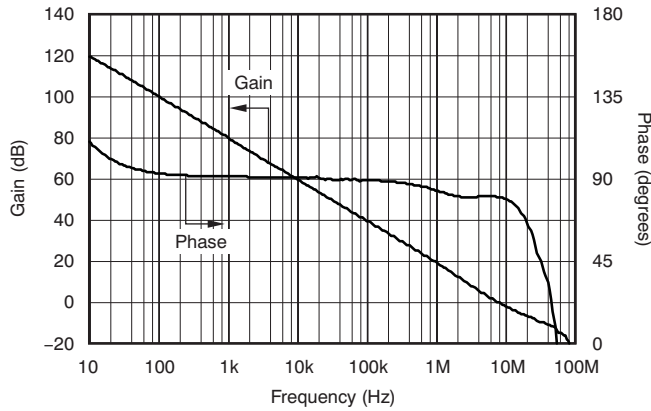


Figure 16.

**CLOSED-LOOP GAIN vs FREQUENCY**

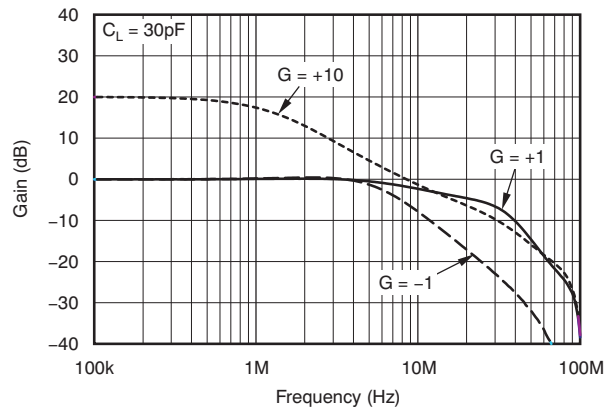


Figure 17.

**OPEN-LOOP GAIN vs TEMPERATURE**

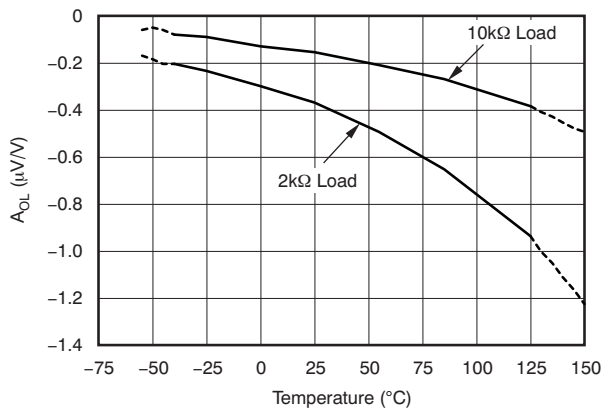


Figure 18.

**OPEN-LOOP OUTPUT IMPEDANCE vs FREQUENCY**

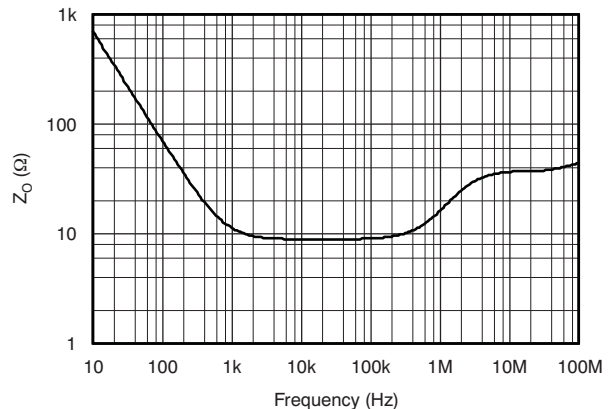


Figure 19.

**TYPICAL CHARACTERISTICS (continued)**

At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

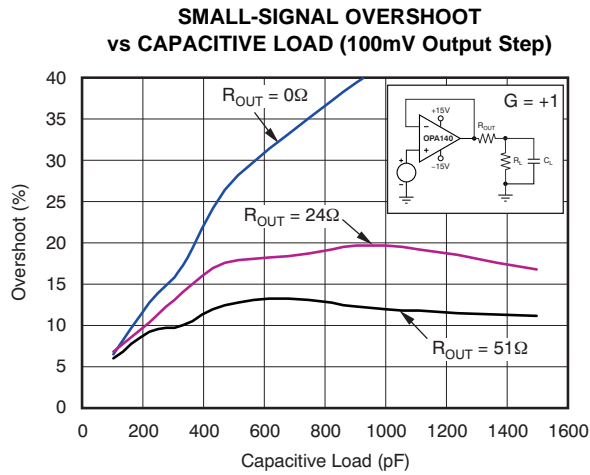


Figure 20.

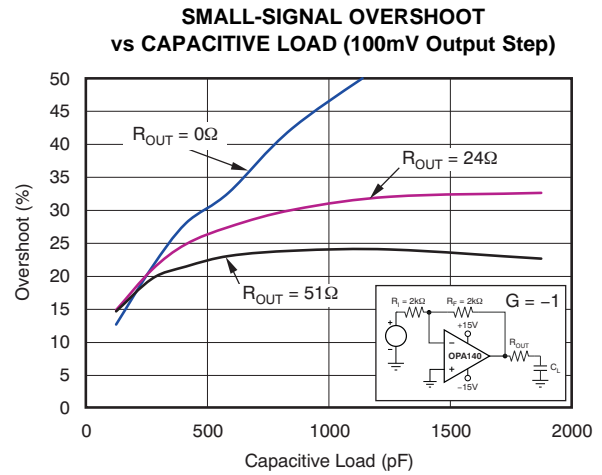


Figure 21.

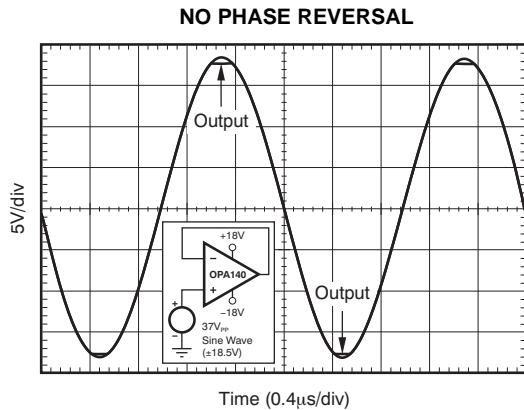


Figure 22.

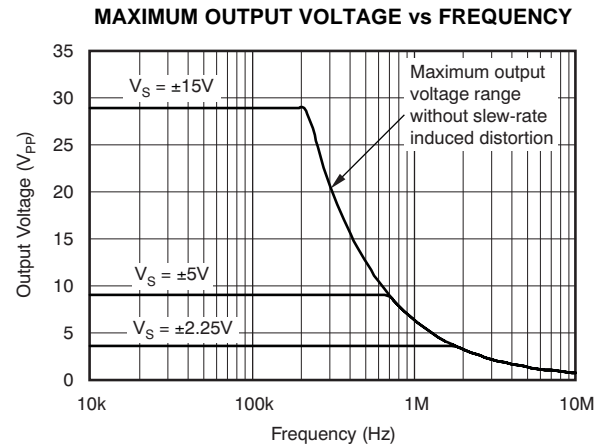


Figure 23.

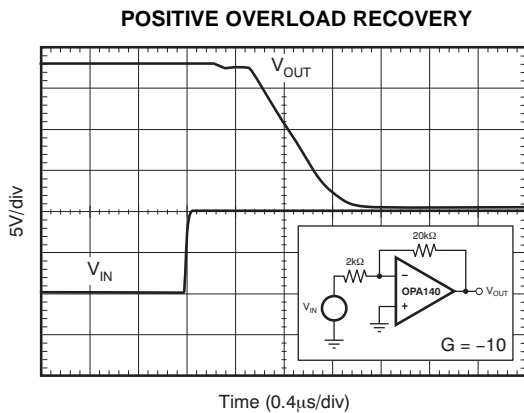


Figure 24.

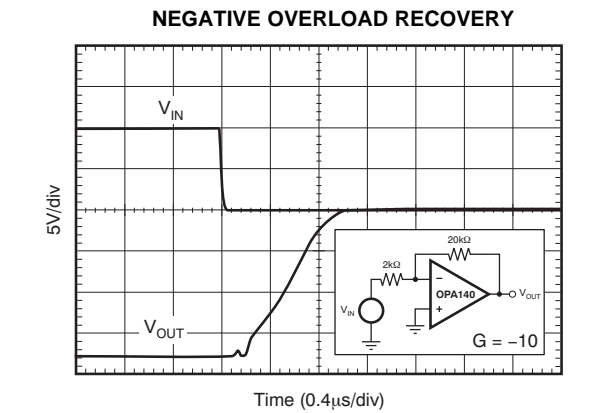


Figure 25.

**TYPICAL CHARACTERISTICS (continued)**

At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

**LARGE-SIGNAL POSITIVE SETTLING TIME  
(10V Step)**

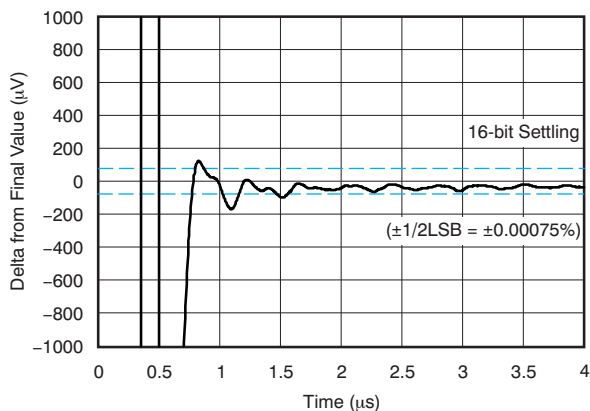


Figure 26.

**LARGE-SIGNAL NEGATIVE SETTLING TIME  
(10V Step)**

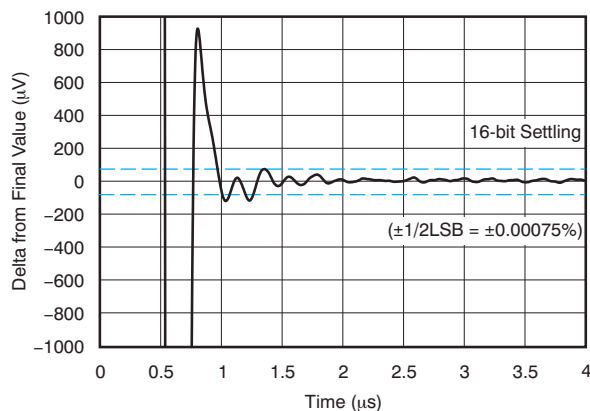


Figure 27.

**SMALL-SIGNAL STEP RESPONSE  
(100mV)**

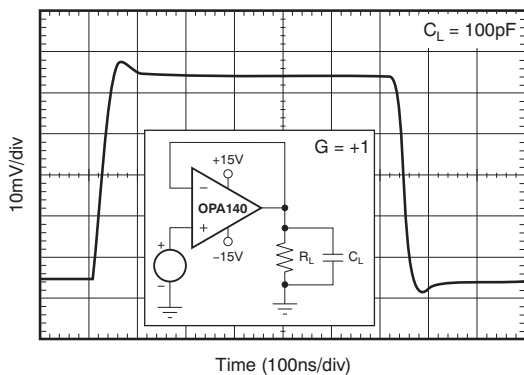


Figure 28.

**SMALL-SIGNAL STEP RESPONSE  
(100mV)**

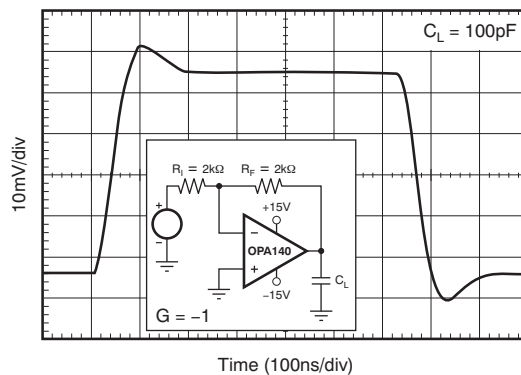


Figure 29.

**LARGE-SIGNAL STEP RESPONSE**

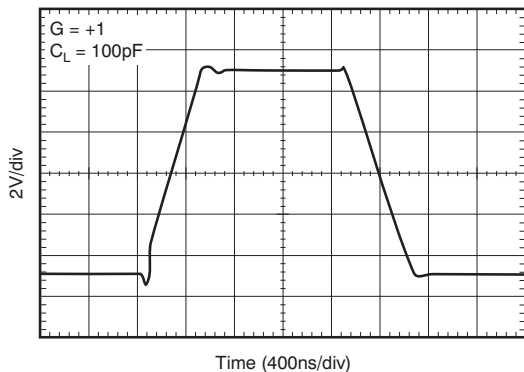


Figure 30.

**LARGE-SIGNAL STEP RESPONSE**

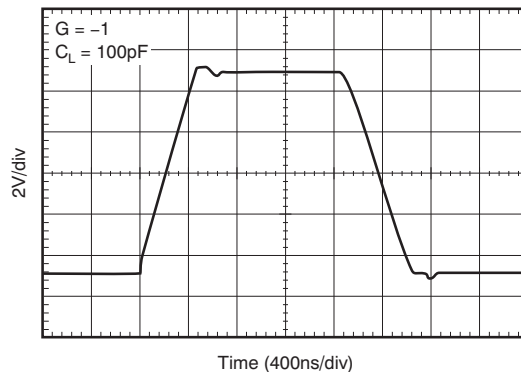


Figure 31.

**TYPICAL CHARACTERISTICS (continued)**

At  $T_A = +25^\circ\text{C}$ ,  $V_S = \pm 18\text{V}$ ,  $R_L = 2\text{k}\Omega$  connected to midsupply,  $V_{CM} = V_{OUT} = \text{midsupply}$ , unless otherwise noted.

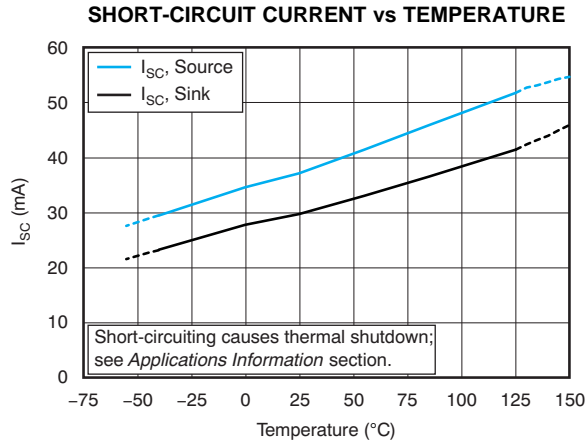


Figure 32.

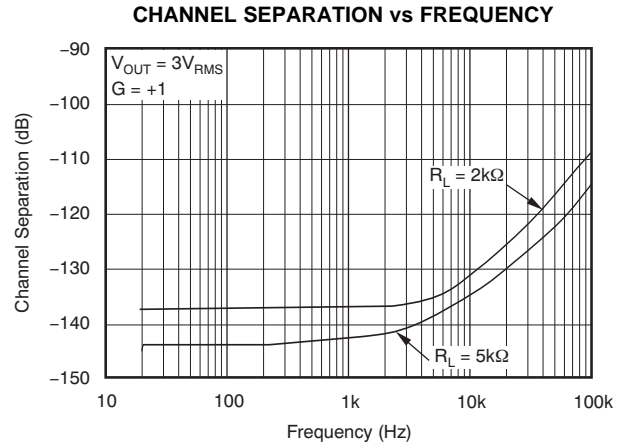


Figure 33.

## APPLICATION INFORMATION

The OPA140, OPA2140, and OPA4140 are unity-gain stable, operational amplifiers with very low noise, input bias current, and input offset voltage. Applications with noisy or high-impedance power supplies require decoupling capacitors placed close to the device pins. In most cases, 0.1µF capacitors are adequate. [Figure 1](#) shows a simplified schematic of the OPA140.

### OPERATING VOLTAGE

The OPA140, OPA2140, and OPA4140 series of op amps can be used with single or dual supplies from an operating range of  $V_S = +4.5V (\pm 2.25V)$  and up to  $V_S = +36V (\pm 18V)$ . These devices do not require symmetrical supplies; they only require a minimum supply voltage of +4.5V ( $\pm 2.25V$ ). For  $V_S$  less than  $\pm 3.5V$ , the common-mode input range does not include midsupply. Supply voltages higher than +40V can permanently damage the device; see the [Absolute Maximum Ratings](#) table. Key parameters are specified over the operating temperature range,  $T_A = -40^\circ C$  to  $+125^\circ C$ . Key parameters that vary over the supply voltage or temperature range are shown in the [Typical Characteristics](#) section of this data sheet.

### CAPACITIVE LOAD AND STABILITY

The dynamic characteristics of the OPAx140 have been optimized for commonly encountered gains, loads, and operating conditions. The combination of low closed-loop gain and high capacitive loads decreases the phase margin of the amplifier and can lead to gain peaking or oscillations. As a result, heavier capacitive loads must be isolated from the output. The simplest way to achieve this isolation is to add a small resistor ( $R_{OUT}$  equal to 50Ω, for example) in series with the output.

[Figure 20](#) and [Figure 21](#) illustrate graphs of *Small-Signal Overshoot vs Capacitive Load* for several values of  $R_{OUT}$ . Also, refer to [Applications Bulletin AB-028](#) (literature number [SBOA015](#), available for download from the [TI web site](#)) for details of analysis techniques and application circuits.

### NOISE PERFORMANCE

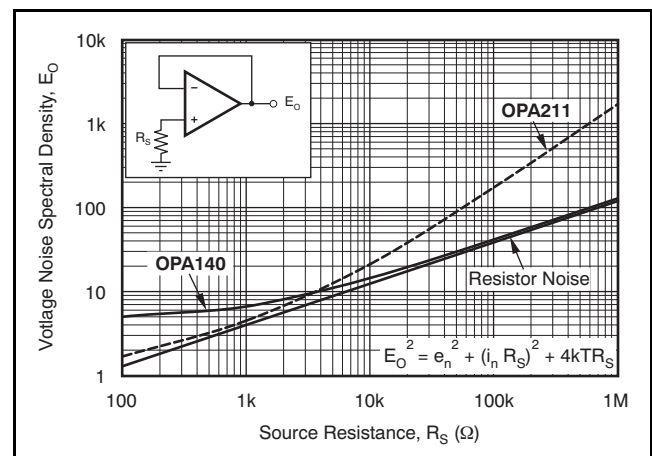
[Figure 34](#) shows the total circuit noise for varying source impedances with the operational amplifier in a unity-gain configuration (with no feedback resistor network and therefore no additional noise contributions). The OPA140 and OPA211 are shown

with total circuit noise calculated. The op amp itself contributes both a voltage noise component and a current noise component. The voltage noise is commonly modeled as a time-varying component of the offset voltage. The current noise is modeled as the time-varying component of the input bias current and reacts with the source resistance to create a voltage component of noise. Therefore, the lowest noise op amp for a given application depends on the source impedance. For low source impedance, current noise is negligible, and voltage noise generally dominates. The OPA140, OPA2140, and OPA4140 family has both low voltage noise and extremely low current noise because of the FET input of the op amp. As a result, the current noise contribution of the OPAx140 series is negligible for any practical source impedance, which makes it the better choice for applications with high source impedance.

The equation in [Figure 34](#) shows the calculation of the total circuit noise, with these parameters:

- $e_n$  = voltage noise
- $I_n$  = current noise
- $R_S$  = source impedance
- $k$  = Boltzmann's constant =  $1.38 \times 10^{-23}$  J/K
- $T$  = temperature in degrees Kelvin (K)

For more details on calculating noise, see the section on [Basic Noise Calculations](#).



**Figure 34. Noise Performance of the OPA140 and OPA211 in Unity-Gain Buffer Configuration**

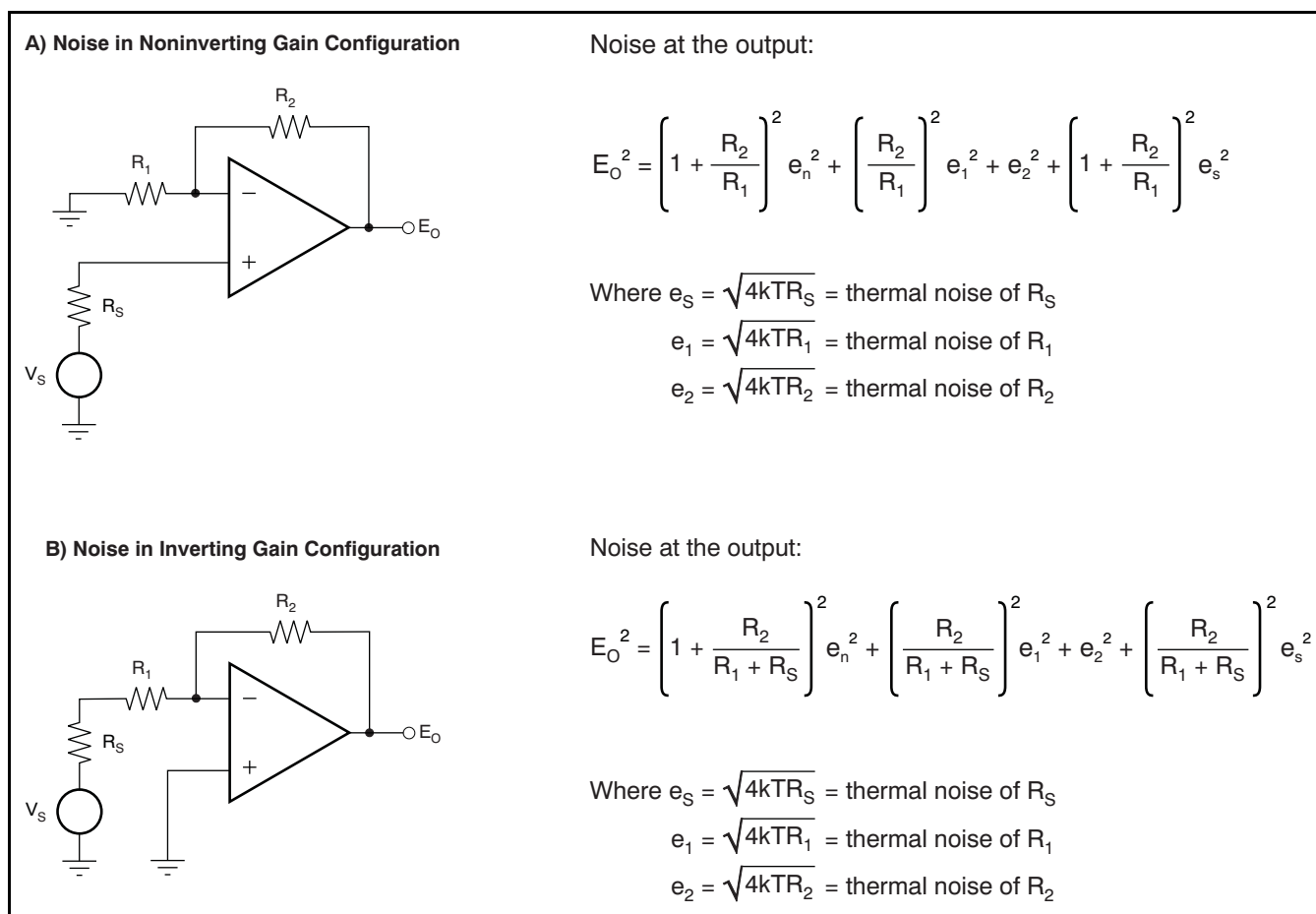
## BASIC NOISE CALCULATIONS

Low-noise circuit design requires careful analysis of all noise sources. External noise sources can dominate in many cases; consider the effect of source resistance on overall op amp noise performance. Total noise of the circuit is the root-sum-square combination of all noise components.

The resistive portion of the source impedance produces thermal noise proportional to the square root of the resistance. This function is plotted in [Figure 34](#). The source impedance is usually fixed; consequently, select the op amp and the feedback resistors to minimize the respective contributions to the total noise.

[Figure 35](#) illustrates both noninverting (A) and inverting (B) op amp circuit configurations with gain. In circuit configurations with gain, the feedback network resistors also contribute noise. In general, the current noise of the op amp reacts with the feedback resistors to create additional noise components. However, the extremely low current noise of the OPAX140 means that its current noise contribution can be neglected.

The feedback resistor values can generally be chosen to make these noise sources negligible. Note that low impedance feedback resistors load the output of the amplifier. The equations for total noise are shown for both configurations.



For the OPAX140 series of operational amplifiers at 1kHz,  $e_n = 5.1\text{nV}/\sqrt{\text{Hz}}$ .

**Figure 35. Noise Calculation in Gain Configurations**

## PHASE-REVERSAL PROTECTION

The OPA140, OPA2140, and OPA4140 family has internal phase-reversal protection. Many FET- and bipolar-input op amps exhibit a phase reversal when the input is driven beyond its linear common-mode range. This condition is most often encountered in noninverting circuits when the input is driven beyond the specified common-mode voltage range, causing the output to reverse into the opposite rail. The input circuitry of the OPA140, OPA2140, and OPA4140 prevents phase reversal with excessive common-mode voltage; instead, the output limits into the appropriate rail (see [Figure 22](#)).

## OUTPUT CURRENT LIMIT

The output current of the OPAx140 series is limited by internal circuitry to +36mA/–30mA (sourcing/sinking), to protect the device if the output is accidentally shorted. This short-circuit current depends on temperature, as shown in [Figure 32](#).

## POWER DISSIPATION AND THERMAL PROTECTION

The OPAx140 series of op amps are capable of driving 2k $\Omega$  loads with power-supply voltages of up to  $\pm 18$ V over the specified temperature range. In a single-supply configuration, where the load is connected to the negative supply voltage, the minimum load resistance is 2.8k $\Omega$  at a supply voltage of +36V. For lower supply voltages (either single-supply or symmetrical supplies), a lower load resistance may be used, as long as the output current does not exceed 13mA; otherwise, the device short-circuit current protection circuit may activate.

Internal power dissipation increases when operating at high supply voltages. Copper leadframe construction used in the OPA140, OPA2140, and OPA4140 series devices improves heat dissipation compared to conventional materials. Printed circuit board (PCB) layout can also help reduce a possible increase in junction temperature. Wide copper traces help dissipate the heat by acting as an additional heatsink. Temperature rise can be further minimized by soldering the devices directly to the PCB rather than using a socket.

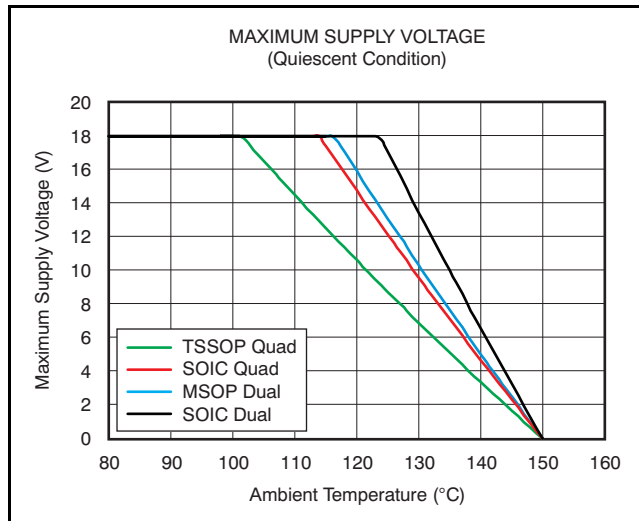
Although the output current is limited by internal protection circuitry, accidental shorting of one or more output channels of a device can result in excessive heating. For instance, when an output is shorted to mid-supply, the typical short-circuit current of 36mA leads to an internal power dissipation of over 600mW at a supply of  $\pm 18$ V.

In the case of a dual OPA2140 in an MSOP-8 package (thermal resistance  $\theta_{JA} = 180^{\circ}\text{C/W}$ ), such power dissipation would lead the die temperature to be 220 $^{\circ}\text{C}$  above ambient temperature, when both channels are shorted. This temperature increase significantly decreases the operating life of the device.

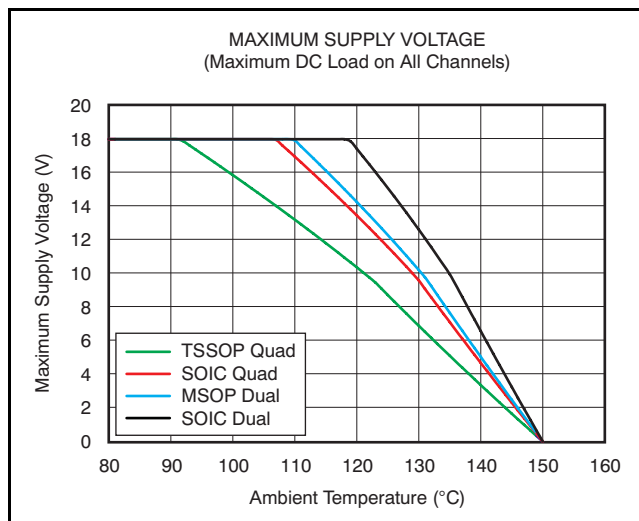
In order to prevent excessive heating, the OPAx140 series has an internal thermal shutdown circuit, which shuts down the device if the die temperature exceeds approximately +180 $^{\circ}\text{C}$ . Once this thermal shutdown circuit activates, a built-in hysteresis of 15 $^{\circ}\text{C}$  ensures that the die temperature must drop to approximately +165 $^{\circ}\text{C}$  before the device switches on again.

Additional consideration should be given to the combination of maximum operating voltage, maximum operating temperature, load, and package type. [Figure 36](#) and [Figure 37](#) show several practical considerations when evaluating the OPA2140 (dual version) and the OPA4140 (quad version).

As an example, the OPA4140 has a maximum total quiescent current of 10.8mA (2.7mA/channel) over temperature. The TSSOP-14 package has a typical thermal resistance of 135 $^{\circ}\text{C/W}$ . This parameter means that because the junction temperature should not exceed +150 $^{\circ}\text{C}$  in order to ensure reliable operation, either the supply voltage must be reduced, or the ambient temperature should remain low enough so that the junction temperature does not exceed +150 $^{\circ}\text{C}$ . This condition is illustrated in [Figure 36](#) for various package types. Moreover, resistive loading of the output causes additional power dissipation and thus self-heating, which also must be considered when establishing the maximum supply voltage or operating temperature. To this end, [Figure 37](#) shows the maximum supply voltage versus temperature for a worst-case dc load resistance of 2k $\Omega$ .



**Figure 36. Maximum Supply Voltage vs Temperature (OPA2140 and OPA4140), Quiescent Condition**



**Figure 37. Maximum Supply Voltage vs Temperature (OPA2140 and OPA4140), Maximum DC Load**

## ELECTRICAL OVERSTRESS

Designers often ask questions about the capability of an operational amplifier to withstand electrical overstress. These questions tend to focus on the device inputs, but may involve the supply voltage pins or even the output pin. Each of these different pin functions have electrical stress limits determined by the voltage breakdown characteristics of the

particular semiconductor fabrication process and specific circuits connected to the pin. Additionally, internal electrostatic discharge (ESD) protection is built into these circuits to protect them from accidental ESD events both before and during product assembly.

It is helpful to have a good understanding of this basic ESD circuitry and its relevance to an electrical overstress event. See [Figure 38](#) for an illustration of the ESD circuits contained in the OPAx140 series (indicated by the dashed line area). The ESD protection circuitry involves several current-steering diodes connected from the input and output pins and routed back to the internal power-supply lines, where they meet at an absorption device internal to the operational amplifier. This protection circuitry is intended to remain inactive during normal circuit operation.

An ESD event produces a short duration, high-voltage pulse that is transformed into a short duration, high-current pulse as it discharges through a semiconductor device. The ESD protection circuits are designed to provide a current path around the operational amplifier core to prevent it from being damaged. The energy absorbed by the protection circuitry is then dissipated as heat.

When an ESD voltage develops across two or more of the amplifier device pins, current flows through one or more of the steering diodes. Depending on the path that the current takes, the absorption device may activate. The absorption device has a trigger, or threshold voltage, that is above the normal operating voltage of the OPAx140 but below the device breakdown voltage level. Once this threshold is exceeded, the absorption device quickly activates and clamps the voltage across the supply rails to a safe level.

When the operational amplifier connects into a circuit such as the one [Figure 38](#) shows, the ESD protection components are intended to remain inactive and not become involved in the application circuit operation. However, circumstances may arise where an applied voltage exceeds the operating voltage range of a given pin. Should this condition occur, there is a risk that some of the internal ESD protection circuits may be biased on, and conduct current. Any such current flow occurs through steering diode paths and rarely involves the absorption device.

Figure 38 depicts a specific example where the input voltage,  $V_{IN}$ , exceeds the positive supply voltage ( $+V_S$ ) by 500mV or more. Much of what happens in the circuit depends on the supply characteristics. If  $+V_S$  can sink the current, one of the upper input steering diodes conducts and directs current to  $+V_S$ . Excessively high current levels can flow with increasingly higher  $V_{IN}$ . As a result, the datasheet specifications recommend that applications limit the input current to 10mA.

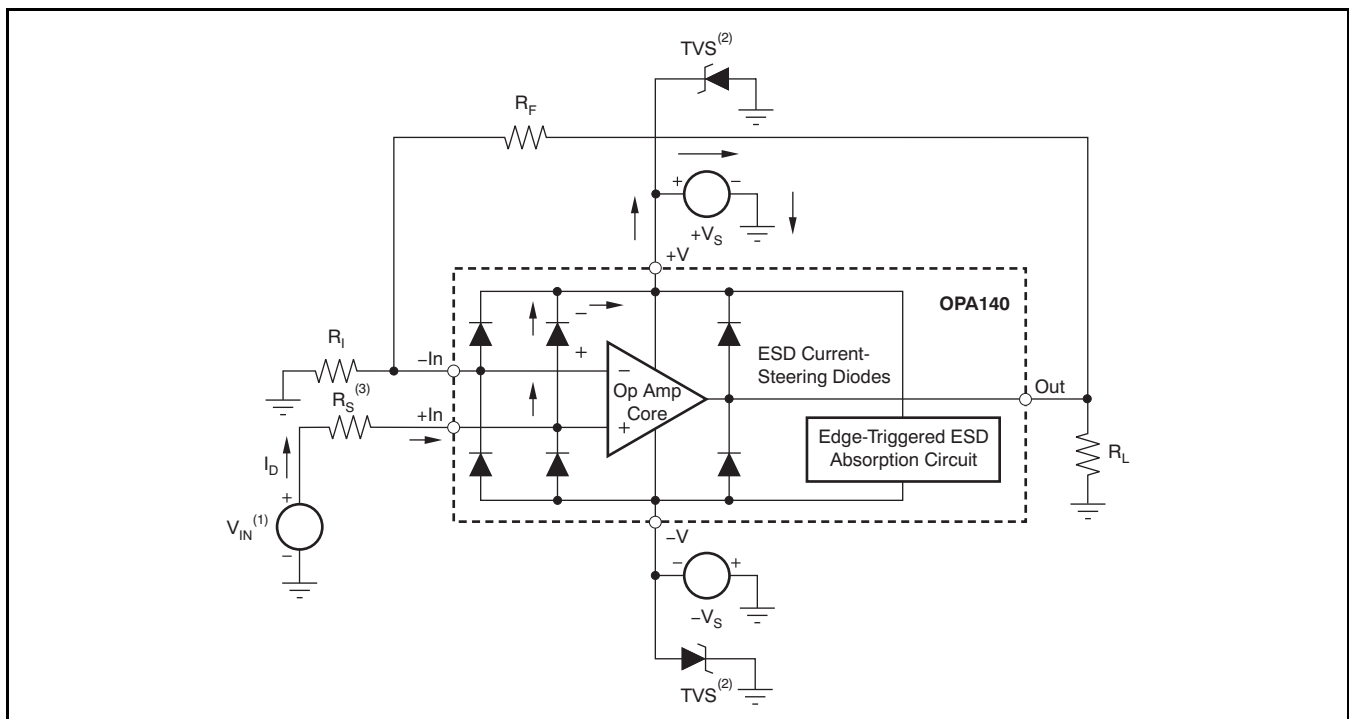
If the supply is not capable of sinking the current,  $V_{IN}$  may begin sourcing current to the operational amplifier, and then take over as the source of positive supply voltage. The danger in this case is that the voltage can rise to levels that exceed the operational amplifier absolute maximum ratings.

Another common question involves what happens to the amplifier if an input signal is applied to the input while the power supplies  $+V_S$  and/or  $-V_S$  are at 0V.

Again, it depends on the supply characteristic while at 0V, or at a level below the input signal amplitude. If the supplies appear as high impedance, then the operational amplifier supply current may be supplied by the input source via the current steering diodes. This state is not a normal bias condition; the amplifier most likely will not operate normally. If the supplies are low impedance, then the current through the steering diodes can become quite high. The current level depends on the ability of the input source to deliver current, and any resistance in the input path.

If there is an uncertainty about the ability of the supply to absorb this current, external zener diodes may be added to the supply pins as shown in Figure 38. The zener voltage must be selected such that the diode does not turn on during normal operation.

However, its zener voltage should be low enough so that the zener diode conducts if the supply pin begins to rise above the safe operating supply voltage level.



- (1)  $V_{IN} = +V_S + 500\text{mV}$ .
- (2) TVS:  $+V_{S(\text{max})} > V_{\text{TVSBR}(\text{Min})} > +V_S$
- (3) Suggested value approximately 1k $\Omega$ .

Figure 38. Equivalent Internal ESD Circuitry and Its Relation to a Typical Circuit Application

**PACKAGING INFORMATION**

Orderable Device	Status <sup>(1)</sup>	Package Type	Package Drawing	Pins	Package Qty	Eco Plan <sup>(2)</sup>	Lead/ Ball Finish	MSL Peak Temp <sup>(3)</sup>	Samples (Requires Login)
OPA140AID	ACTIVE	SOIC	D	8	75	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA140AIDBVR	ACTIVE	SOT-23	DBV	5	3000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA140AIDBVT	ACTIVE	SOT-23	DBV	5	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA140AIDGKR	ACTIVE	MSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA140AIDGKT	ACTIVE	MSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA140AIDR	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA2140AID	ACTIVE	SOIC	D	8	75	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA2140AIDGKR	ACTIVE	MSOP	DGK	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA2140AIDGKT	ACTIVE	MSOP	DGK	8	250	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA2140AIDR	ACTIVE	SOIC	D	8	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA4140AID	ACTIVE	SOIC	D	14	50	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR	
OPA4140AIDR	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-3-260C-168 HR	
OPA4140AIPW	ACTIVE	TSSOP	PW	14	90	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	
OPA4140AIPWR	ACTIVE	TSSOP	PW	14	2000	Green (RoHS & no Sb/Br)	CU NIPDAU	Level-2-260C-1 YEAR	

<sup>(1)</sup> The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

<sup>(2)</sup> Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

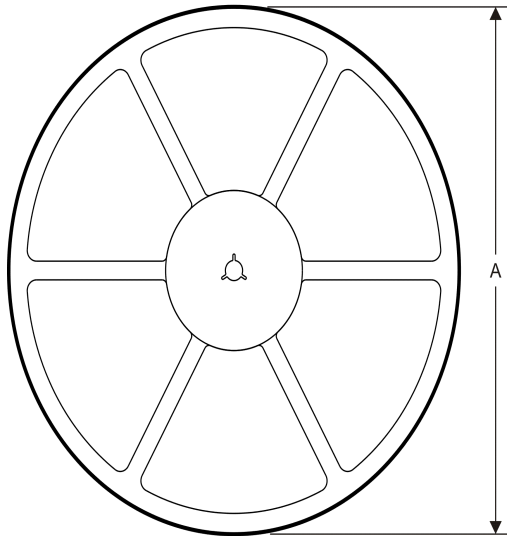
**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

<sup>(3)</sup> MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

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**TAPE AND REEL INFORMATION**
**REEL DIMENSIONS**

**TAPE DIMENSIONS**


A0	Dimension designed to accommodate the component width
B0	Dimension designed to accommodate the component length
K0	Dimension designed to accommodate the component thickness
W	Overall width of the carrier tape
P1	Pitch between successive cavity centers

**TAPE AND REEL INFORMATION**

\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
OPA140AIDBVR	SOT-23	DBV	5	3000	180.0	8.4	3.23	3.17	1.37	4.0	8.0	Q3
OPA140AIDBVT	SOT-23	DBV	5	250	180.0	8.4	3.23	3.17	1.37	4.0	8.0	Q3
OPA140AIDGKR	MSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA140AIDGKT	MSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA140AIDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA2140AIDGKR	MSOP	DGK	8	2500	330.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA2140AIDGKT	MSOP	DGK	8	250	180.0	12.4	5.3	3.4	1.4	8.0	12.0	Q1
OPA2140AIDR	SOIC	D	8	2500	330.0	12.4	6.4	5.2	2.1	8.0	12.0	Q1
OPA4140AIDR	SOIC	D	14	2500	330.0	16.4	6.5	9.0	2.1	8.0	16.0	Q1
OPA4140AIPWR	TSSOP	PW	14	2000	330.0	12.4	6.9	5.6	1.6	8.0	12.0	Q1

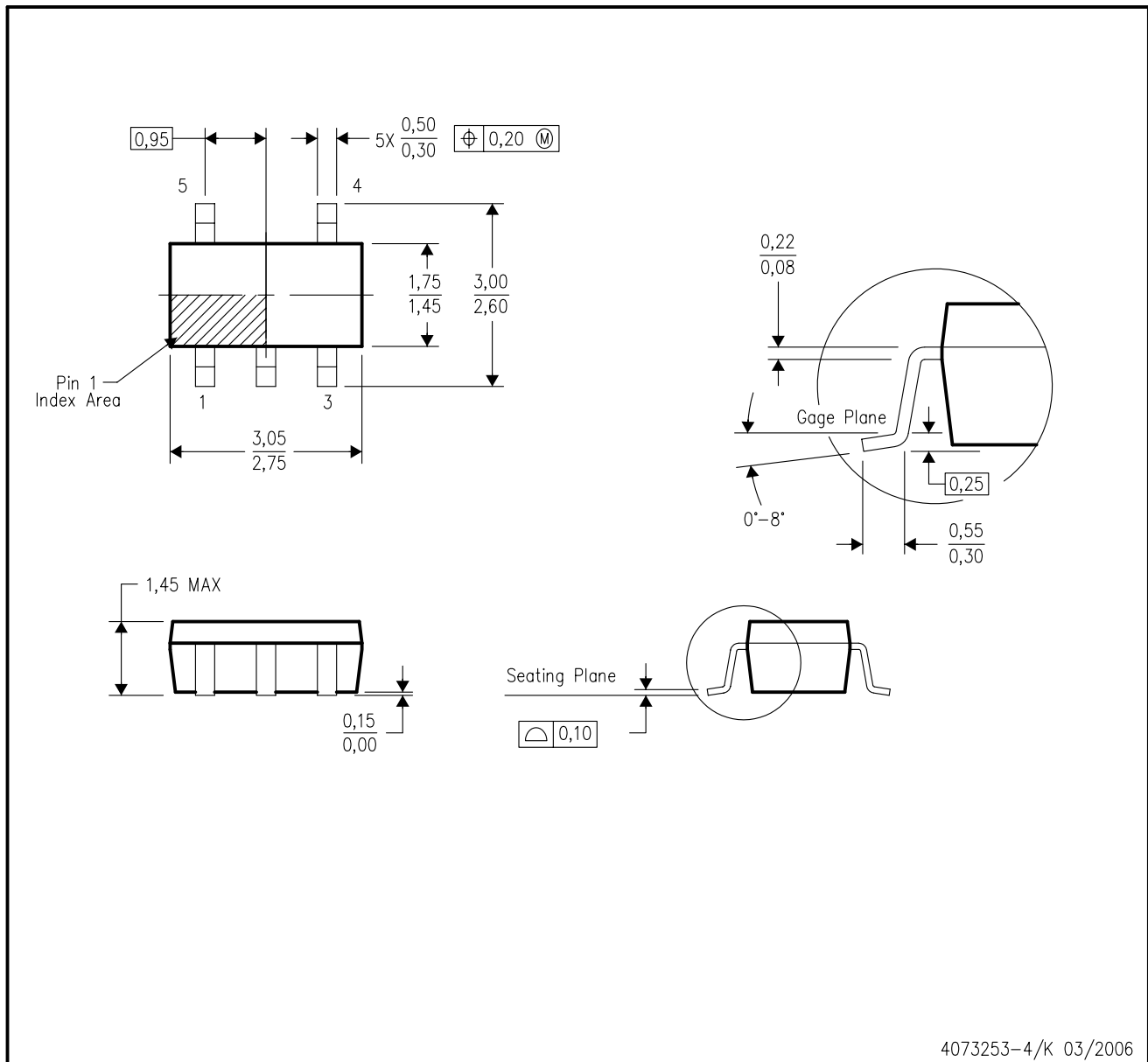
**TAPE AND REEL BOX DIMENSIONS**


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
OPA140AIDBVR	SOT-23	DBV	5	3000	202.0	201.0	28.0
OPA140AIDBVT	SOT-23	DBV	5	250	202.0	201.0	28.0
OPA140AIDGKR	MSOP	DGK	8	2500	346.0	346.0	29.0
OPA140AIDGKT	MSOP	DGK	8	250	210.0	185.0	35.0
OPA140AIDR	SOIC	D	8	2500	346.0	346.0	29.0
OPA2140AIDGKR	MSOP	DGK	8	2500	346.0	346.0	29.0
OPA2140AIDGKT	MSOP	DGK	8	250	210.0	185.0	35.0
OPA2140AIDR	SOIC	D	8	2500	346.0	346.0	29.0
OPA4140AIDR	SOIC	D	14	2500	346.0	346.0	33.0
OPA4140AIPWR	TSSOP	PW	14	2000	346.0	346.0	29.0

DBV (R-PDSO-G5)

PLASTIC SMALL-OUTLINE PACKAGE



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Body dimensions do not include mold flash or protrusion. Mold flash and protrusion shall not exceed 0.15 per side.
  - D. Falls within JEDEC MO-178 Variation AA.

DBV (R-PDSO-G5)

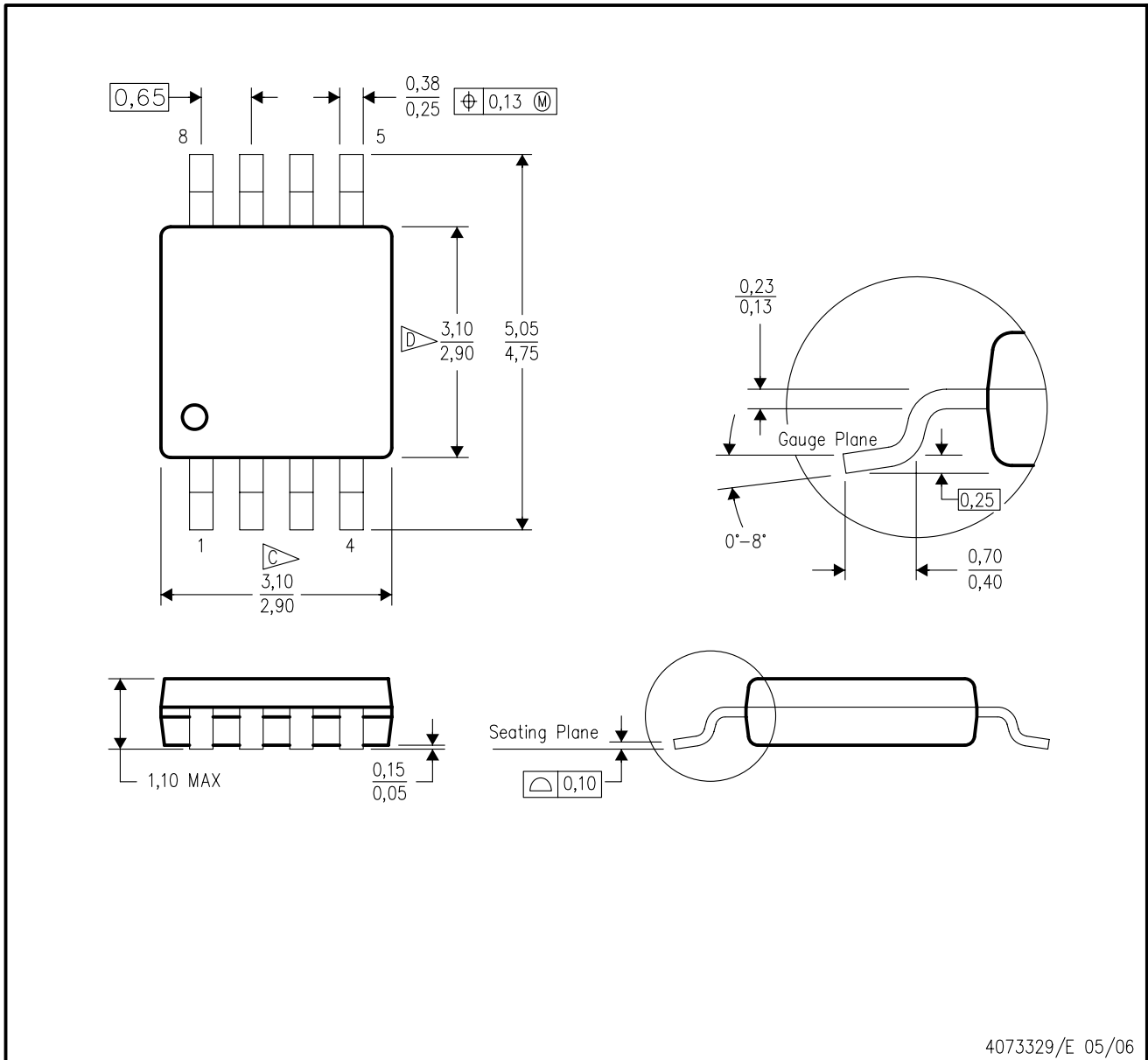
PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Customers should place a note on the circuit board fabrication drawing not to alter the center solder mask defined pad.
  - D. Publication IPC-7351 is recommended for alternate designs.
  - E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.

DGK (S-PDSO-G8)

PLASTIC SMALL-OUTLINE PACKAGE



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.15 per end.
  - D. Body width does not include interlead flash. Interlead flash shall not exceed 0.50 per side.
  - E. Falls within JEDEC MO-187 variation AA, except interlead flash.

D (R-PDSO-G14)

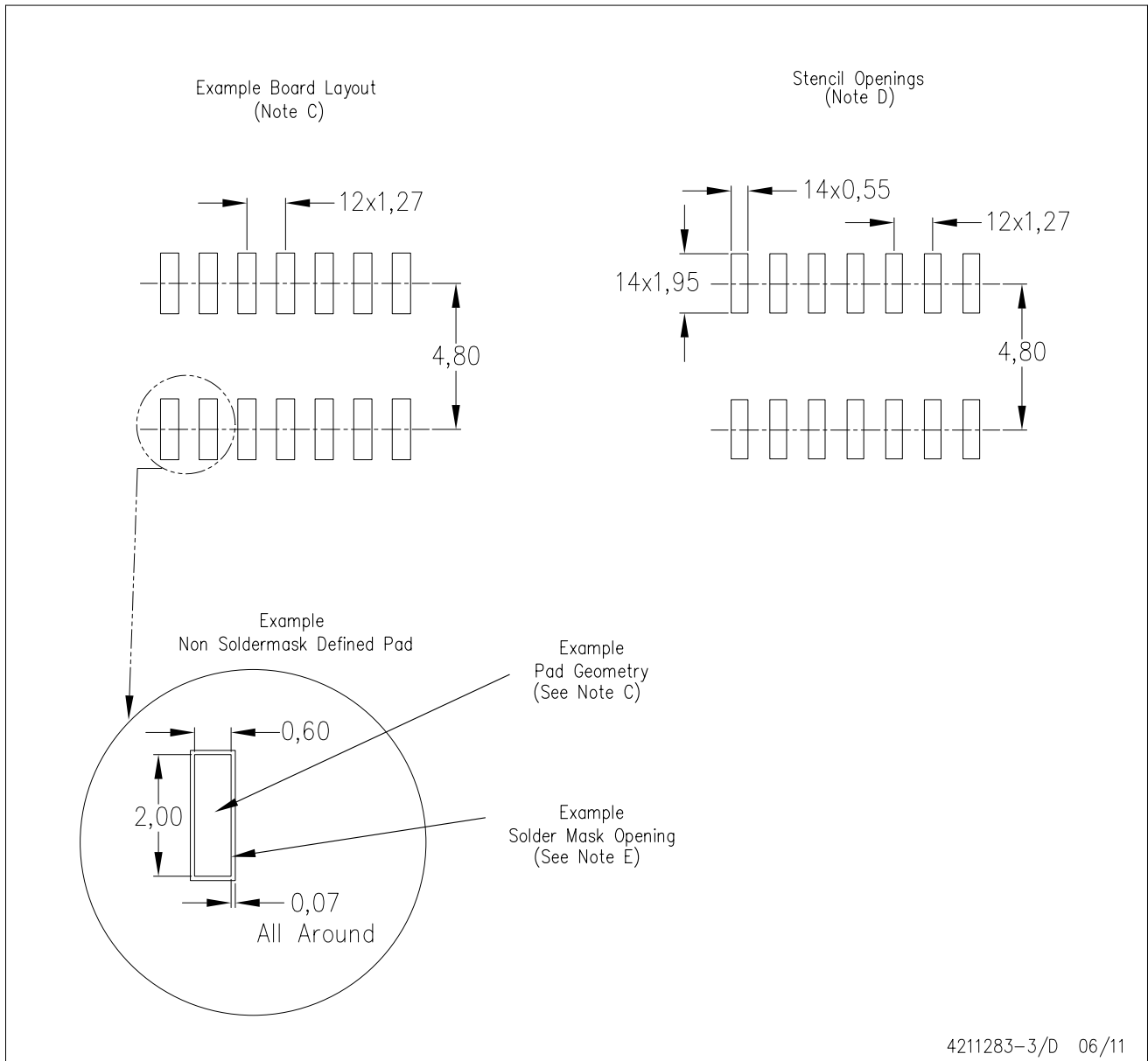
PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  - $\triangle C$  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
  - $\triangle D$  Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
  - E. Reference JEDEC MS-012 variation AB.

D (R-PDSO-G14)

PLASTIC SMALL OUTLINE

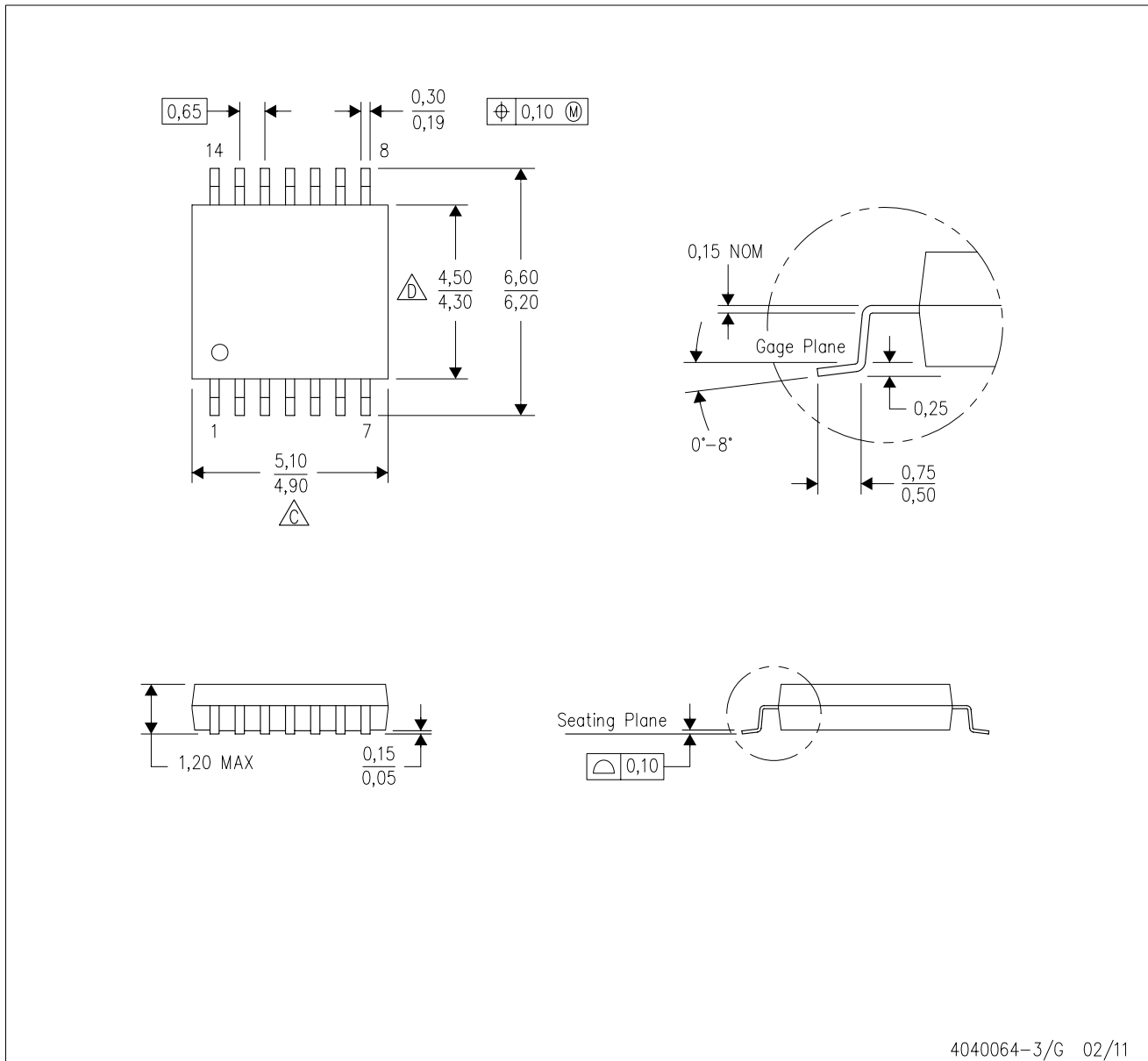


4211283-3/D 06/11



- NOTES:
- A. All linear dimensions are in millimeters.
  - B. This drawing is subject to change without notice.
  - C. Publication IPC-7351 is recommended for alternate designs.
  - D. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - E. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE

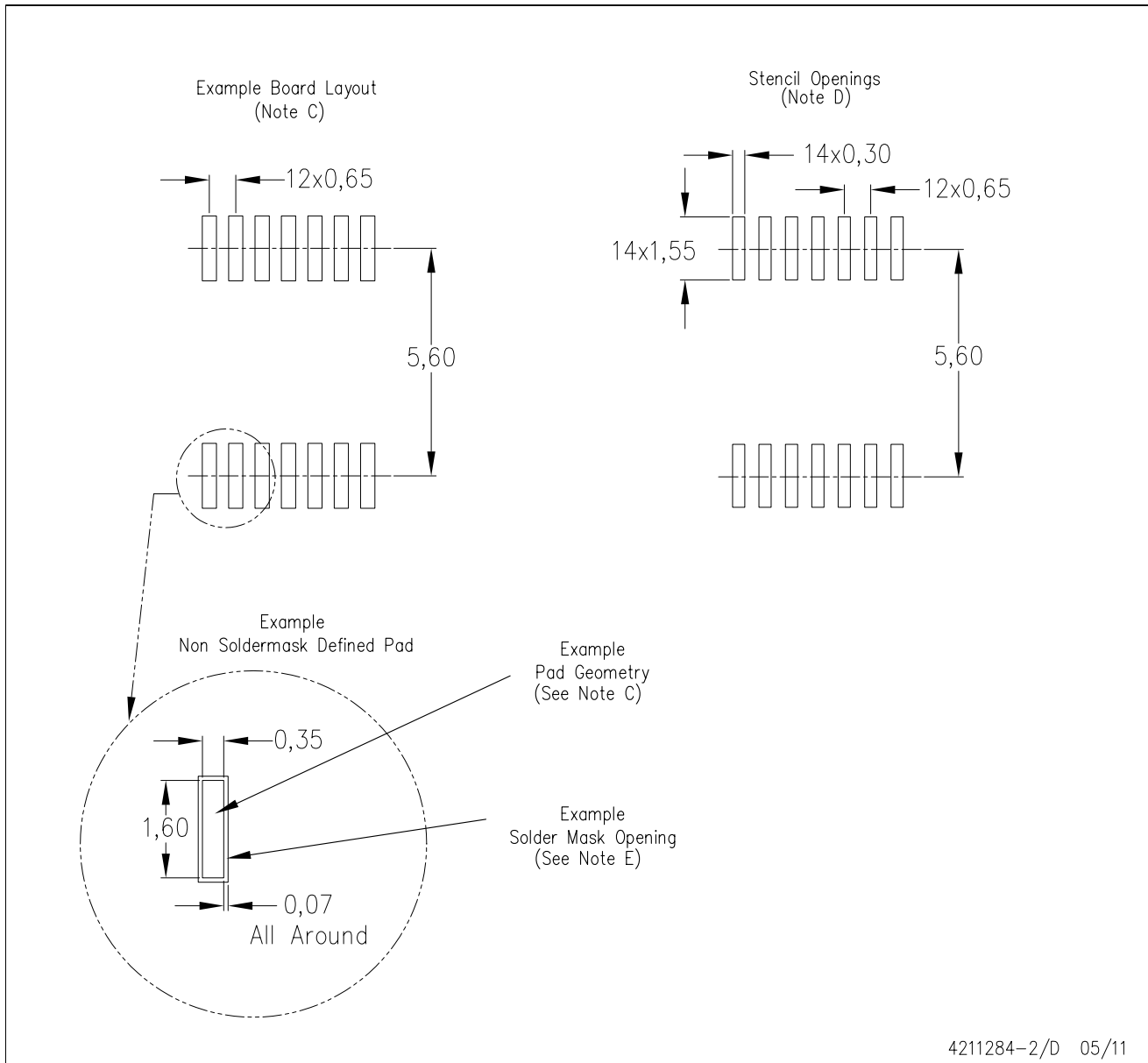


4040064-3/G 02/11

- NOTES:
- A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
  - B. This drawing is subject to change without notice.
  -  C. Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0,15 each side.
  -  D. Body width does not include interlead flash. Interlead flash shall not exceed 0,25 each side.
  - E. Falls within JEDEC MO-153

PW (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

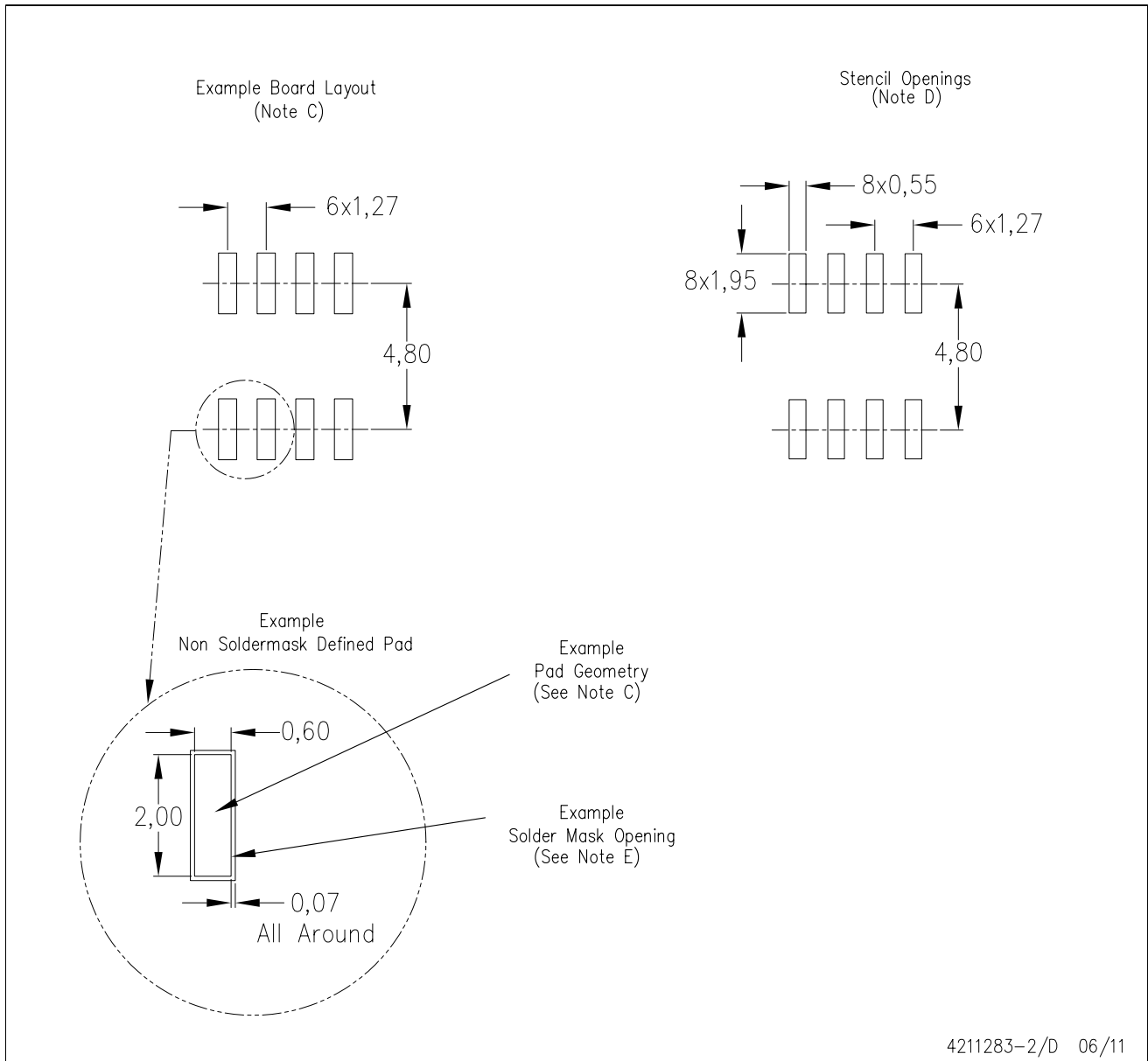
D (R-PDSO-G8)

PLASTIC SMALL OUTLINE



D (R-PDSO-G8)

PLASTIC SMALL OUTLINE



- NOTES:
- All linear dimensions are in millimeters.
  - This drawing is subject to change without notice.
  - Publication IPC-7351 is recommended for alternate designs.
  - Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Refer to IPC-7525 for other stencil recommendations.
  - Customers should contact their board fabrication site for solder mask tolerances between and around signal pads.

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Mailing Address: Texas Instruments, Post Office Box 655303, Dallas, Texas 75265  
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